

4.1.2 Saturated Ketones, C₇ - C₈**2,2-Dimethyl-3-pentanone**

[564-04-5]

C₇H₁₄O

MW = 114.19

174

Table 1. Fit with estimated B coefficient for 5 accepted points. Deviation $\sigma_w = 0.227$.

Coefficient	$\rho = A + BT$
A	1070.69
B	-0.880

Table 2. Experimental values with uncertainties and deviation from calculated values.

T K	$\rho_{\text{exp}} \pm 2\sigma_{\text{est}}$ kg · m ⁻³	$\rho_{\text{exp}} - \rho_{\text{calc}}$ kg · m ⁻³	Ref.	T K	$\rho_{\text{exp}} \pm 2\sigma_{\text{est}}$ kg · m ⁻³	$\rho_{\text{exp}} - \rho_{\text{calc}}$ kg · m ⁻³	Ref.
273.15	831.0 ± 3.0	0.68	1875-wis ¹⁾	293.15	812.5 ± 1.0	-0.22	1913-fav
294.15	808.0 ± 3.0	-3.84	1875-wis ¹⁾	298.15	799.3 ± 3.0	-8.99	1931-pfe/adk ¹⁾
273.15	825.7 ± 3.0	-4.62	1900-mar ¹⁾	293.15	811.9 ± 1.0	-0.82	1960-pet/sok
293.15	810.5 ± 3.0	-2.22	1900-mar ¹⁾	293.15	812.8 ± 0.4	0.08	1970-sel
273.15	830.3 ± 1.0	-0.02	1913-fav	298.15	808.4 ± 0.4	0.08	1970-sel

¹⁾ Not included in calculation of linear coefficients.**Table 3.** Recommended values.

T K	$\rho_{\text{exp}} \pm 2\sigma_{\text{est}}$ kg · m ⁻³
270.00	833.1 ± 1.3
280.00	824.3 ± 0.8
290.00	815.5 ± 0.5
293.15	812.7 ± 0.4
298.15	808.3 ± 0.5

2,4-Dimethyl-3-pentanone

[565-80-0]

C₇H₁₄O

MW = 114.19

175

Table 1. Coefficients of the polynomial expansion equation. Standard deviations (see introduction): $\sigma_{c,w} = 1.2191$ (combined temperature ranges, weighted), $\sigma_{c,uw} = 2.7592 \cdot 10^{-1}$ (combined temperature ranges, unweighted).

Coefficient	$T = 273.15 \text{ to } 348.15 \text{ K}$ $\rho = A + BT + CT^2 + DT^3 + \dots$
A	$1.06190 \cdot 10^3$
B	$-8.78647 \cdot 10^{-1}$

cont.

2,4-Dimethyl-3-pentanone (cont.)

Table 2. Experimental values with uncertainties and deviation from calculated values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref. (Symbol in Fig. 1)	$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref. (Symbol in Fig. 1)
298.15	799.73 ± 0.60	-0.20	1931-pfe/adk(×)	348.15	756.00 ± 1.00	-0.00	1942-say/bax(×)
283.15	813.90 ± 1.00	0.79	1942-say/bax(×)	293.15	803.00 ± 0.40	-1.33	1949-dre/mar(○)
298.15	801.10 ± 1.00	1.17	1942-say/bax(×)	298.15	798.61 ± 0.40	-1.32	1949-dre/mar(○)
303.15	796.80 ± 1.00	1.26	1942-say/bax(×)	293.15	803.00 ± 0.40	-1.33	1952-coo(Δ)
313.15	786.90 ± 1.00	0.15	1942-say/bax(×)	273.15	823.30 ± 0.50	1.40	1960-wri(∇)
323.15	779.20 ± 1.00	1.23	1942-say/bax(×)	273.15	823.30 ± 0.50	1.40	1961-wri(◆)
328.15	773.40 ± 1.00	-0.17	1942-say/bax(×)	293.15	803.00 ± 0.40	-1.33	1970-sel(□)
338.15	764.50 ± 1.00	-0.29	1942-say/bax(×)	298.15	798.50 ± 0.40	-1.43	1970-sel(□)

Further references: [1876-mun, 1914-low, 1914-mur/amo, 1925-ter, 1940-gin/plo, 1954-bau/jon].

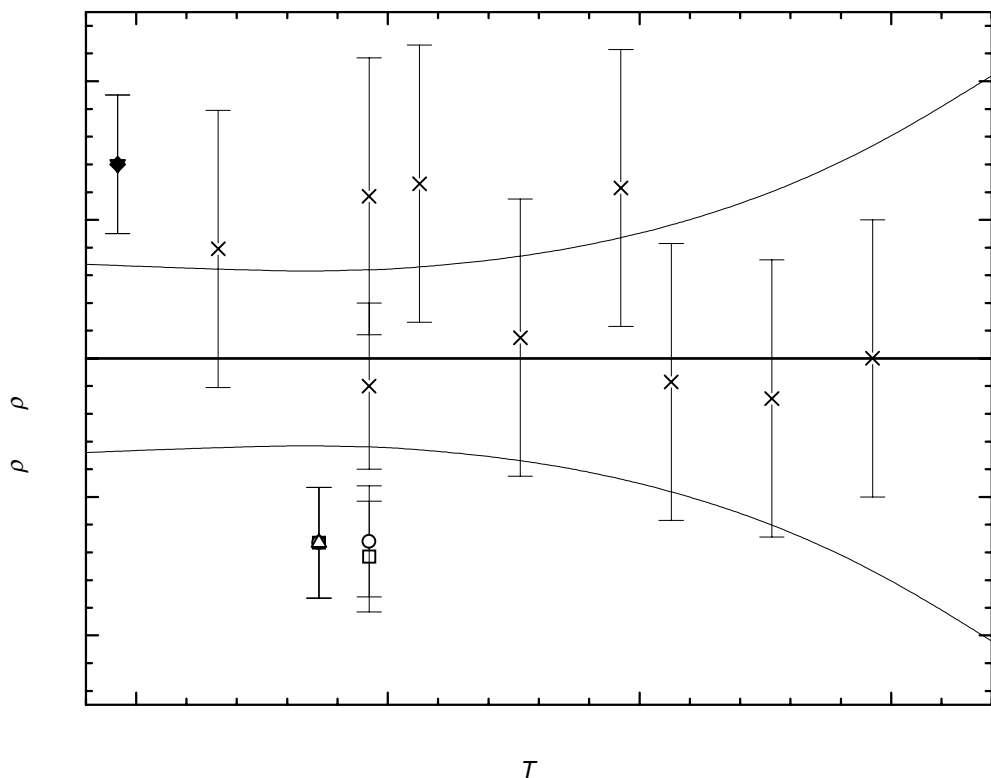


Fig. 1. The symbols show the deviation of the calculated from the experimental values from Table 2. The curves above and below the zero line indicate the calculated error region of the recommended values given in Table 3. The error bars represent the experimental errors. (Error bars smaller than the symbols are omitted for clarity of the figure.)

cont.

Table 3. Recommended values (fit to the reliable experimental values according to the equations $\rho = A + BT + CT^2 + DT^3 + \dots$ or $\rho = [1 + 1.75(1 - T/T_c)^{1/3} + 0.75(1 - T/T_c)][\rho_c + A(T_c - T) + B(T_c - T)^2 + C(T_c - T)^3 + D(T_c - T)^4]$).

$\frac{T}{K}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{T}{K}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{T}{K}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$
270.00	824.67 ± 0.68	298.15	799.93 ± 0.64	330.00	771.95 ± 0.99
280.00	815.88 ± 0.65	300.00	798.31 ± 0.64	340.00	763.16 ± 1.24
290.00	807.09 ± 0.63	310.00	789.52 ± 0.70	350.00	754.37 ± 1.59
293.15	804.33 ± 0.63	320.00	780.73 ± 0.81	360.00	745.59 ± 2.04

3,3-Dimethyl-2-pentanone

[20669-04-9]

C₇H₁₄O

MW = 114.19

176

Table 1. Fit with estimated B coefficient for 3 accepted points. Deviation $\sigma_w = 0.405$.

Coefficient	$\rho = A + BT$
A	1099.62
B	-0.940

Table 2. Experimental values with uncertainties and deviation from calculated values.

$\frac{T}{K}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
273.15	842.0 ± 2.0	-0.86	1875-wis
294.15	823.0 ± 2.0	-0.12	1875-wis
293.15	824.3 ± 1.0	0.24	1913-mee

Table 3. Recommended values.

$\frac{T}{K}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$
270.00	845.8 ± 2.5
280.00	836.4 ± 1.8
290.00	827.0 ± 1.5
293.15	824.1 ± 1.6
298.15	819.4 ± 1.7

3,4-Dimethyl-2-pentanone

[565-78-6]

C₇H₁₄O

MW = 114.19

177

Table 1. Experimental and recommended values with uncertainties.

$\frac{T}{K}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
287.15	825.0 ± 2.0	1939-col/mos ¹⁾
293.15	827.3 ± 1.0	1955-mes/pet
293.15	827.3 ± 1.0	Recommended

¹⁾ Not included in calculation of recommended value.

4,4-Dimethyl-2-pentanone**[590-50-1]****C₇H₁₄O****MW = 114.19****178****Table 1.** Experimental and recommended values with uncertainties.

T K	$\rho_{\text{exp}} \pm 2\sigma_{\text{est}}$ kg · m ⁻³	Ref.
298.15	801.2 ± 2.0	1931-pfe/adk ¹⁾
293.15	811.2 ± 3.0	1963-kup/pet ¹⁾
293.15	804.0 ± 0.5	1952-coo
293.15	804.0 ± 0.5	Recommended

¹⁾ Not included in calculation of recommended value.**3-Ethyl-2-pentanone****[6137-03-7]****C₇H₁₄O****MW = 114.19****179****Table 1.** Experimental and recommended values with uncertainties.

T K	$\rho_{\text{exp}} \pm 2\sigma_{\text{est}}$ kg · m ⁻³	Ref.
295.15	815.3 ± 3.0	1866-fra/dup ¹⁾
293.15	818.6 ± 3.0	1890-gar ¹⁾
292.15	823.0 ± 2.0	1907-fou/tif ¹⁾
289.15	825.0 ± 2.0	1927-col ¹⁾
288.15	823.0 ± 3.0	1927-sui/pol ¹⁾
293.15	823.0 ± 1.0	1960-pla/mel
293.15	823.0 ± 1.0	Recommended

¹⁾ Not included in calculation of recommended value.**2-Heptanone****[110-43-0]****C₇H₁₄O****MW = 114.19****180****Table 1.** Coefficients of the polynomial expansion equation. Standard deviations (see introduction): $\sigma_{\text{c,w}} = 7.7780 \cdot 10^{-1}$ (combined temperature ranges, weighted), $\sigma_{\text{c,uw}} = 1.4335 \cdot 10^{-1}$ (combined temperature ranges, unweighted).

Coefficient	$T = 253.15 \text{ to } 413.15 \text{ K}$ $\rho = A + BT + CT^2 + DT^3 + \dots$
<i>A</i>	$1.00396 \cdot 10^3$
<i>B</i>	$-4.28202 \cdot 10^{-1}$
<i>C</i>	$-7.26099 \cdot 10^{-4}$

cont.

Table 2. Experimental values with uncertainties and deviation from calculated values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref. (Symbol in Fig. 1)	$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref. (Symbol in Fig. 1)
273.15	832.37 ± 0.30	-0.45	1929-sim(O)	373.15	742.20 ± 0.50	-0.87	1941-col(X)
288.15	819.64 ± 0.30	-0.64	1929-sim(O)	393.15	722.50 ± 0.50	-0.88	1941-col(X)
303.15	806.78 ± 0.30	-0.64	1929-sim(O)	308.00	803.50 ± 0.50	0.31	1942-owe/qua(X)
413.15	702.40 ± 0.50	-0.71	1941-col(X)	323.30	790.10 ± 0.50	0.47	1942-owe/qua(X)
297.95	811.80 ± 0.50	-0.12	1942-owe/qua(X)	283.15	824.50 ± 0.50	0.00	1942-say/bax(X)
288.15	819.64 ± 0.40	-0.64	1936-ceu(Δ)	303.15	807.20 ± 0.50	-0.22	1942-say/bax(X)
303.15	806.73 ± 0.40	-0.69	1936-ceu(Δ)	323.15	789.80 ± 0.50	0.04	1942-say/bax(X)
293.15	811.10 ± 0.50	-4.93	1940-cow/jef ¹⁾	333.15	780.90 ± 0.50	0.19	1942-say/bax(X)
334.85	779.90 ± 0.50	0.74	1940-cow/jef(X)	338.15	776.10 ± 0.50	-0.04	1942-say/bax(X)
358.05	759.70 ± 0.50	2.14	1940-cow/jef(X)	348.15	767.60 ± 0.50	0.73	1942-say/bax(X)
253.15	851.30 ± 0.50	2.27	1941-col(X)	293.15	815.30 ± 0.50	-0.73	1952-coo(X)
273.15	834.00 ± 0.50	1.18	1941-col(X)	293.15	815.68 ± 0.30	-0.35	1952-pom(□)
293.15	816.60 ± 0.50	0.57	1941-col(X)	298.15	811.64 ± 0.30	-0.10	1952-pom(□)
313.15	798.90 ± 0.50	0.24	1941-col(X)	273.15	832.40 ± 0.40	-0.42	1960-wri(♦)
333.15	780.60 ± 0.50	-0.11	1941-col(X)	273.15	832.40 ± 0.50	-0.42	1961-wri(X)
353.15	762.00 ± 0.50	-0.18	1941-col(X)	298.15	811.10 ± 0.40	-0.64	1988-gar/cob(V)

¹⁾ Not included in Fig. 1.

Further references: [1865-pop, 1888-beh-1, 1927-sui/pol, 1930-err/she, 1930-she, 1938-tho/cam, 1940-gin/plo, 1951-str/boy, 1954-doo, 1963-iva/dol, 1966-mey/wag, 1968-ano].

Table 3. Recommended values (fit to the reliable experimental values according to the equations $\rho = A + BT + CT^2 + DT^3 + \dots$ or $\rho = [1 + 1.75(1 - T/T_c)^{1/3} + 0.75(1 - T/T_c)][\rho_c + A(T_c - T) + B(T_c - T)^2 + C(T_c - T)^3 + D(T_c - T)^4]$).

$\frac{T}{\text{K}}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{T}{\text{K}}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{T}{\text{K}}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$
250.00	851.53 ± 0.60	300.00	810.15 ± 0.43	370.00	746.12 ± 0.56
260.00	843.54 ± 0.54	310.00	801.44 ± 0.43	380.00	736.39 ± 0.60
270.00	835.41 ± 0.49	320.00	792.58 ± 0.44	390.00	726.52 ± 0.66
280.00	827.14 ± 0.46	330.00	783.58 ± 0.45	400.00	716.50 ± 0.73
290.00	818.72 ± 0.44	340.00	774.43 ± 0.47	410.00	706.34 ± 0.81
293.15	816.03 ± 0.44	350.00	765.14 ± 0.49	420.00	696.03 ± 0.91
298.15	811.74 ± 0.43	360.00	755.70 ± 0.52		

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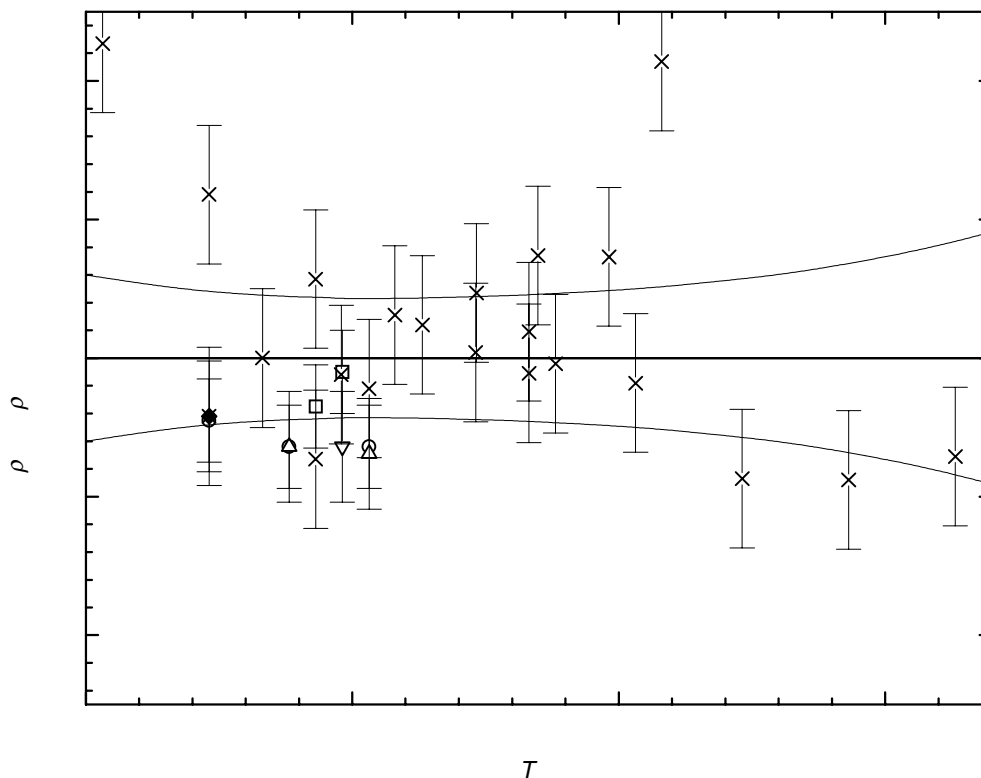
2-Heptanone (cont.)

Fig. 1. The symbols show the deviation of the calculated from the experimental values from Table 2. The curves above and below the zero line indicate the calculated error region of the recommended values given in Table 3. The error bars represent the experimental errors. (Error bars smaller than the symbols are omitted for clarity of the figure.)

3-Heptanone

[106-35-4]

C₇H₁₄O

MW = 114.19

181

Table 1. Coefficients of the polynomial expansion equation. Standard deviations (see introduction): $\sigma_{c,w} = 4.2892 \cdot 10^{-1}$ (combined temperature ranges, weighted), $\sigma_{c,uw} = 2.2874 \cdot 10^{-1}$ (combined temperature ranges, unweighted).

Coefficient	T = 288.15 to 359.65 K
	$\rho = A + BT + CT^2 + DT^3 + \dots$
A	$9.33902 \cdot 10^2$
B	$-1.10979 \cdot 10^{-2}$
C	$-1.30437 \cdot 10^{-3}$

cont.

Table 2. Experimental values with uncertainties and deviation from calculated values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref. (Symbol in Fig. 1)	$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref. (Symbol in Fig. 1)
295.15	816.70 ± 0.40	-0.30	1930-err/she(○)	313.65	800.80 ± 0.60	-1.30	1948-vog-7(◆)
288.15	822.20 ± 0.30	-0.20	1930-she(×)	335.05	782.90 ± 0.60	-0.86	1948-vog-7(◆)
293.15	818.30 ± 0.30	-0.26	1930-she(×)	359.65	761.10 ± 0.60	-0.09	1948-vog-7(◆)
297.95	816.30 ± 1.00	1.50	1942-owe/qua(×)	298.15	816.20 ± 1.00	1.56	1950-ada/van(×)
308.00	807.70 ± 1.00	0.95	1942-owe/qua(×)	293.15	818.70 ± 0.40	0.14	1952-coo(□)
323.30	794.10 ± 1.00	0.12	1942-owe/qua(×)	293.15	818.20 ± 0.60	-0.36	1954-doo(Δ)
293.15	818.10 ± 0.60	-0.46	1948-vog-7(◆)	293.15	818.10 ± 0.60	-0.46	1968-ano(∇)

Further references: [1934-von/man, 1991-lor/jim-1].

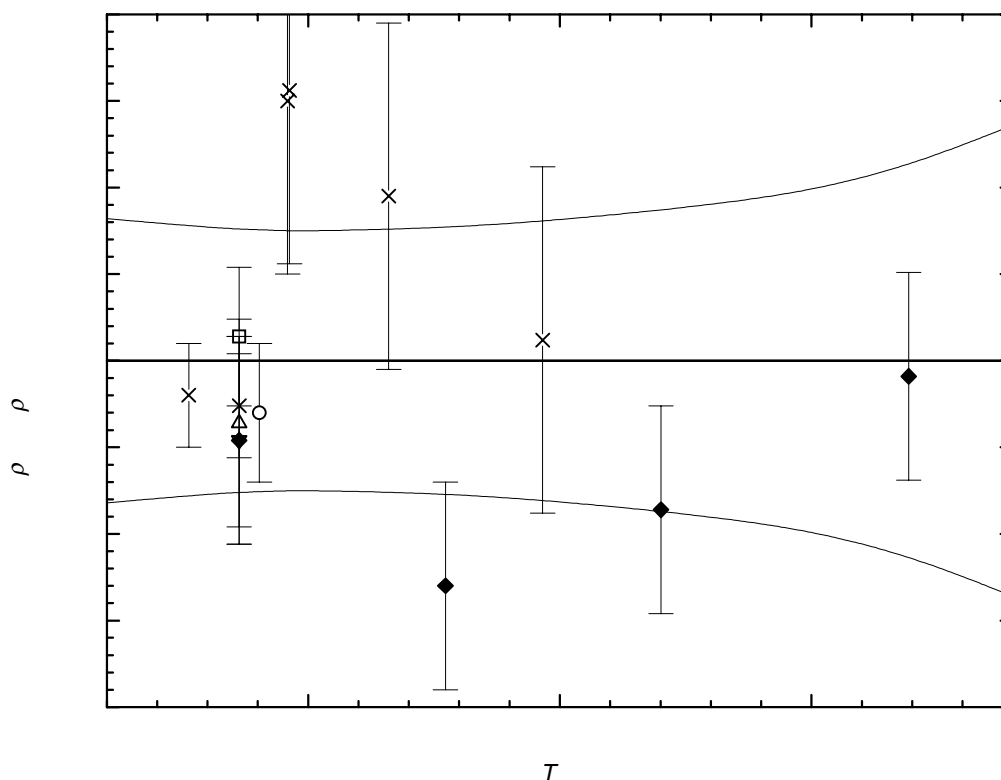


Fig. 1. The symbols show the deviation of the calculated from the experimental values from Table 2. The curves above and below the zero line indicate the calculated error region of the recommended values given in Table 3. The error bars represent the experimental errors. (Error bars smaller than the symbols are omitted for clarity of the figure.)

cont.

3-Heptanone (cont.)**Table 3.** Recommended values (fit to the reliable experimental values according to the equations

$$\rho = A + BT + CT^2 + DT^3 + \dots \text{ or } \rho = [1 + 1.75(1 - T/T_c)^{1/3} + 0.75(1 - T/T_c)][\rho_c + A(T_c - T) + B(T_c - T)^2 + C(T_c - T)^3 + D(T_c - T)^4].$$

$\frac{T}{\text{K}}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{T}{\text{K}}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{T}{\text{K}}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$
280.00	828.53 ± 0.82	300.00	813.18 ± 0.75	340.00	779.34 ± 0.90
290.00	820.99 ± 0.77	310.00	805.11 ± 0.76	350.00	770.23 ± 0.98
293.15	818.56 ± 0.76	320.00	796.78 ± 0.79	360.00	760.86 ± 1.13
298.15	814.64 ± 0.75	330.00	788.19 ± 0.84	370.00	751.23 ± 1.36

4-Heptanone

[123-19-3]

C₇H₁₄O

MW = 114.19

182

Table 1. Coefficients of the polynomial expansion equation. Standard deviations (see introduction):

$\sigma_{c,w} = 7.7897 \cdot 10^{-1}$ (combined temperature ranges, weighted), $\sigma_{c,uw} = 1.9425 \cdot 10^{-1}$ (combined temperature ranges, unweighted).

Coefficient	T = 253.15 to 393.15 K $\rho = A + BT + CT^2 + DT^3 + \dots$
A	$1.00729 \cdot 10^3$
B	$-4.29768 \cdot 10^{-1}$
C	$-7.52768 \cdot 10^{-4}$

Table 2. Experimental values with uncertainties and deviation from calculated values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref. (Symbol in Fig. 1)	$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref. (Symbol in Fig. 1)
288.25	820.50 ± 0.70	-0.36	1893-eyk(×)	293.15	816.10 ± 0.50	-0.51	1941-col(Δ)
287.95	820.30 ± 1.00	-0.82	1896-per(×)	298.15	811.60 ± 0.50	-0.63	1941-col(Δ)
363.15	753.40 ± 1.00	1.46	1896-per(×)	313.15	798.00 ± 0.50	-0.89	1941-col(Δ)
363.15	753.33 ± 1.00	1.39	1896-per(×)	333.15	780.60 ± 0.50	0.04	1941-col(Δ)
295.15	816.00 ± 0.60	1.14	1930-err/she(×)	353.15	762.00 ± 0.50	0.37	1941-col(Δ)
288.15	821.20 ± 0.60	0.25	1930-she(∇)	373.15	741.00 ± 0.50	-1.10	1941-col(Δ)
293.15	817.50 ± 0.60	0.89	1930-she(∇)	393.15	721.60 ± 0.50	-0.37	1941-col(Δ)
293.15	814.50 ± 1.00	-2.11	1940-cow/jef ¹⁾	303.15	808.10 ± 0.60	0.28	1942-say/bax(◆)
314.65	796.40 ± 1.00	-1.13	1940-cow/jef(×)	323.15	791.30 ± 0.60	1.50	1942-say/bax(◆)
335.65	778.30 ± 1.00	0.07	1940-cow/jef(×)	343.15	770.20 ± 0.60	-0.97	1942-say/bax(◆)
360.65	755.90 ± 1.00	1.52	1940-cow/jef(×)	293.15	815.10 ± 0.50	-1.51	1952-coo(○)
253.15	850.60 ± 0.50	0.35	1941-col(Δ)	298.15	811.40 ± 0.50	-0.83	1988-gar/cob(□)
273.15	833.60 ± 0.50	-0.13	1941-col(Δ)				

¹⁾ Not included in Fig. 1.

Further references: [1888-beh, 1890-gar, 1894-bru-1, 1914-low, 1940-sch/ipa, 1942-owe/qua, 1947-tuo/guy, 1952-sha/whi, 1956-shu/bel, 1957-wid/phi].

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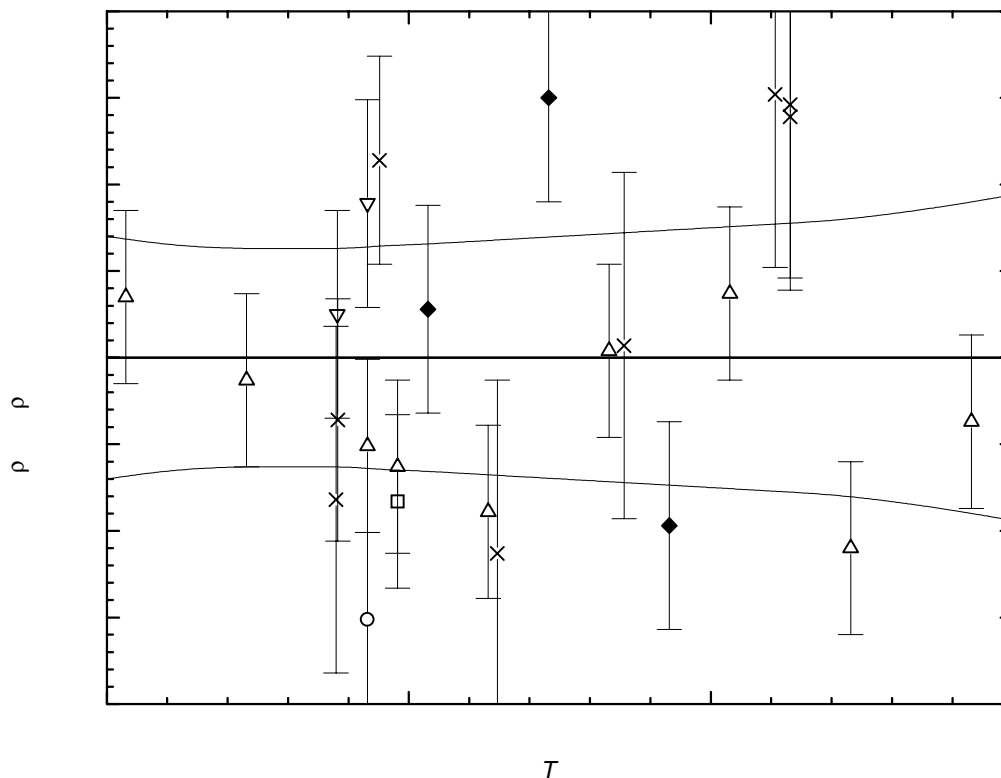


Fig. 1. The symbols show the deviation of the calculated from the experimental values from Table 2. The curves above and below the zero line indicate the calculated error region of the recommended values given in Table 3. The error bars represent the experimental errors. (Error bars smaller than the symbols are omitted for clarity of the figure.)

Table 3. Recommended values (fit to the reliable experimental values according to the equations $\rho = A + BT + CT^2 + DT^3 + \dots$ or $\rho = [1 + 1.75(1 - T/T_c)^{1/3} + 0.75(1 - T/T_c)][\rho_c + A(T_c - T) + B(T_c - T)^2 + C(T_c - T)^3 + D(T_c - T)^4]$).

$\frac{T}{\text{K}}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{T}{\text{K}}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{T}{\text{K}}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$
250.00	852.80 ± 0.70	298.15	812.23 ± 0.65	350.00	764.65 ± 0.75
260.00	844.66 ± 0.65	300.00	810.61 ± 0.65	360.00	755.01 ± 0.77
270.00	836.37 ± 0.63	310.00	801.72 ± 0.67	370.00	745.22 ± 0.79
280.00	827.93 ± 0.63	320.00	792.68 ± 0.69	380.00	735.27 ± 0.83
290.00	819.35 ± 0.63	330.00	783.49 ± 0.71	390.00	725.18 ± 0.88
293.15	816.61 ± 0.64	340.00	774.15 ± 0.73	400.00	714.94 ± 0.94

2-Methyl-3-hexanone

[7379-12-6]

C₇H₁₄O

MW = 114.19

183

Table 1. Experimental value with uncertainty.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
288.15	821.6 ± 1.0	1927-sui/pol

3-Methyl-2-hexanone [2550-21-2] C₇H₁₄O MW = 114.19 184

Table 1. Experimental and recommended values with uncertainties.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
293.15	865.8 ± 6.0	1890-gar ¹⁾
298.15	828.0 ± 2.0	1933-pow/mur
298.15	828.0 ± 2.0	Recommended

¹⁾ Not included in calculation of recommended value.

4-Methyl-2-hexanone [105-42-0] C₇H₁₄O MW = 114.19 185

Table 1. Experimental value with uncertainty.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
298.15	808.5 ± 1.0	1930-dav/dix

4-Methyl-3-hexanone [17042-16-9] C₇H₁₄O MW = 114.19 186

Table 1. Experimental and recommended values with uncertainties.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
292.15	824.8 ± 3.0	1907-fou/tif ¹⁾
293.15	816.2 ± 3.0	1948-hus/goe ¹⁾
298.15	824.0 ± 2.0	1954-dub/luf-1
298.15	824.0 ± 2.0	Recommended

¹⁾ Not included in calculation of recommended value.

5-Methyl-2-hexanone [110-12-3] C₇H₁₄O MW = 114.19 187

Table 1. Experimental and recommended values with uncertainties.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
290.35	817.5 ± 2.0	1877-roh ¹⁾
290.35	816.5 ± 4.0	1878-roh ¹⁾
293.15	812.0 ± 0.6	1955-ano-13
293.15	811.6 ± 0.6	1968-ano
293.15	811.8 ± 0.6	Recommended

¹⁾ Not included in calculation of recommended value.

5-Methyl-3-hexanone [623-56-3] C₇H₁₄O MW = 114.19 188

Table 1. Fit with estimated B coefficient for 3 accepted points. Deviation $\sigma_w = 0.180$.

Coefficient	$\rho = A + BT$
A	1058.36
B	-0.840

Table 2. Experimental values with uncertainties and deviation from calculated values.

T K	$\rho_{\text{exp}} \pm 2\sigma_{\text{est}}$ kg · m ⁻³	$\rho_{\text{exp}} - \rho_{\text{calc}}$ kg · m ⁻³	Ref.
273.15	829.0 ± 2.0	0.09	1891-wag
290.15	815.0 ± 2.0	0.37	1891-wag
293.15	812.0 ± 1.0	-0.11	1957-shu/bel

Table 3. Recommended values.

T K	$\rho_{\text{exp}} \pm 2\sigma_{\text{est}}$ kg · m ⁻³
270.00	831.6 ± 2.4
280.00	823.2 ± 1.8
290.00	814.8 ± 1.5
293.15	812.1 ± 1.5
298.15	807.9 ± 1.7

2,2-Dimethyl-3-hexanone [5405-79-8] C₈H₁₆O MW = 128.21 189

Table 1. Fit with estimated B coefficient for 2 accepted points. Deviation $\sigma_w = 0.115$.

Coefficient	$\rho = A + BT$
A	1060.86
B	-0.840

Table 2. Experimental values with uncertainties and deviation from calculated values.

T K	$\rho_{\text{exp}} \pm 2\sigma_{\text{est}}$ kg · m ⁻³	$\rho_{\text{exp}} - \rho_{\text{calc}}$ kg · m ⁻³	Ref.
298.15	810.5 ± 0.6	0.12	1913-hal/bau
290.15	822.5 ± 3.0	5.37	1921-ler ¹⁾
293.15	814.5 ± 0.6	-0.11	1960-pet/sok

¹⁾ Not included in calculation of linear coefficients.

(cont.)

2,2-Dimethyl-3-hexanone (cont.)**Table 3.** Recommended values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$
290.00	817.3 ± 0.7
293.15	814.6 ± 0.5
298.15	810.4 ± 0.5

2,5-Dimethyl-3-hexanone

[1888-57-9]

C₈H₁₆O

MW = 128.21

190

Table 1. Fit with estimated *B* coefficient for 2 accepted points. Deviation $\sigma_w = 0.590$.

Coefficient	$\rho = A + BT$
<i>A</i>	1046.03
<i>B</i>	-0.800

Table 2. Experimental values with uncertainties and deviation from calculated values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
287.15	865.0 ± 3.0	48.69	1879-car ¹⁾
287.15	865.0 ± 3.0	48.69	1900-car-1 ¹⁾
273.15	826.9 ± 1.0	-0.59	1913-fav
293.15	812.1 ± 1.0	0.59	1913-fav

¹⁾ Not included in calculation of linear coefficients.**Table 3.** Recommended values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$
270.00	830.0 ± 1.5
280.00	822.0 ± 0.8
290.00	814.0 ± 1.0
293.15	811.5 ± 1.2
298.15	807.5 ± 1.7

3,3-Dimethyl-2-hexanone

[26118-38-7]

C₈H₁₆O

MW = 128.21

191

Table 1. Fit with estimated *B* coefficient for 2 accepted points. Deviation $\sigma_w = 0.250$.

Coefficient	$\rho = A + BT$
<i>A</i>	1059.97
<i>B</i>	-0.800

cont.

Table 2. Experimental values with uncertainties and deviation from calculated values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
293.15	825.7 ± 1.0	0.25	1957-bol/ego-1
273.15	841.2 ± 1.0	-0.25	1957-bol/ego-1

Table 3. Recommended values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$
270.00	844.0 ± 1.1
280.00	836.0 ± 0.9
290.00	828.0 ± 1.0
293.15	825.5 ± 1.1
298.15	821.5 ± 1.2

3,4-Dimethyl-2-hexanone

[19550-10-8]

C₈H₁₆O

MW = 128.21

192

Table 1. Experimental values with uncertainties.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
295.15	829.5 ± 0.8	1931-pow/sec
288.15	832.0 ± 2.0	1935-col-1

4,4-Dimethyl-2-hexanone

[40239-18-7]

C₈H₁₆O

MW = 128.21

193

Table 1. Experimental value with uncertainty.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
293.15	829.0 ± 2.0	1934-dra/kli

4,4-Dimethyl-3-hexanone

[19550-14-2]

C₈H₁₆O

MW = 128.21

194

Table 1. Experimental and recommended values with uncertainties.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
273.15	841.8 ± 2.0	1875-wis ¹⁾
294.15	844.9 ± 2.0	1875-wis ¹⁾
293.15	829.8 ± 1.0	1922-nyb
293.15	829.8 ± 1.0	Recommended

¹⁾ Not included in calculation of recommended value.

5,5-Dimethyl-3-hexanone [5340-30-7] C₈H₁₆O MW = 128.21 195

Table 1. Experimental value with uncertainty.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
293.15	812.0 ± 2.0	1933-whi/lau

3-Ethyl-2-hexanone [6137-05-9] C₈H₁₆O MW = 128.21 196

Table 1. Experimental value with uncertainty.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
293.15	830.8 ± 1.0	1890-gar

3-Ethyl-3-methyl-2-pentanone [19780-65-5] C₈H₁₆O MW = 128.21 197

Table 1. Experimental value with uncertainty.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
293.15	838.9 ± 0.6	1922-nyb

2-Methyl-3-heptanone [13019-20-0] C₈H₁₆O MW = 128.21 198

Table 1. Experimental and recommended values with uncertainties.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
285.15	820.9 ± 3.0	1912-pic/ken ¹⁾
293.15	817.5 ± 0.6	1914-low
293.15	816.0 ± 2.0	1914-wal-1
293.15	817.4 ± 0.7	Recommended

¹⁾ Not included in calculation of recommended value.

2-Methyl-4-heptanone [626-33-5] C₈H₁₆O MW = 128.21 199

Table 1. Experimental value with uncertainty.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
293.15	816.2 ± 1.0	1957-shu/bel

3-Methyl-4-heptanone [15726-15-5] C₈H₁₆O MW = 128.21 200

Table 1. Experimental value with uncertainty.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
298.15	817.0 ± 2.0	1939-stu/adk

4-Methyl-3-heptanone [6137-11-7] C₈H₁₆O MW = 128.21 201

Table 1. Experimental value with uncertainty.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
298.15	820.0 ± 2.0	1954-dub/luf-1

5-Methyl-2-heptanone [18217-12-4] C₈H₁₆O MW = 128.21 202

Table 1. Fit with estimated *B* coefficient for 3 accepted points. Deviation $\sigma_w = 0.373$.

Coefficient	$\rho = A + BT$
<i>A</i>	1055.32
<i>B</i>	-0.820

Table 2. Experimental values with uncertainties and deviation from calculated values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
293.15	815.1 ± 1.0	0.17	1908-bue-1
298.15	811.0 ± 2.0	0.17	1963-col/bru
298.15	810.0 ± 2.0	-0.83	1963-col/bru

Table 3. Recommended values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$
290.00	817.5 ± 1.6
293.15	814.9 ± 1.5
298.15	810.8 ± 1.6

5-Methyl-3-heptanone [541-85-5] C₈H₁₆O MW = 128.21 203

Table 1. Experimental value with uncertainty.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
297.15	829.0 ± 2.0	1931-pow/sec

6-Methyl-2-heptanone [928-68-7] C₈H₁₆O MW = 128.21 204

Table 1. Experimental values with uncertainties.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
292.15	816.5 ± 1.0	1911-wal
298.15	810.0 ± 2.0	1962-col/bru

2-Octanone [111-13-7] C₈H₁₆O MW = 128.21 205

Table 1. Coefficients of the polynomial expansion equation. Standard deviations (see introduction):

$\sigma_{\text{c,w}} = 7.8918 \cdot 10^{-1}$ (combined temperature ranges, weighted), $\sigma_{\text{c,uw}} = 1.5651 \cdot 10^{-1}$ (combined temperature ranges, unweighted).

Coefficient	T = 253.15 to 433.15 K $\rho = A + BT + CT^2 + DT^3 + \dots$
A	$1.02615 \cdot 10^3$
B	$-5.67318 \cdot 10^{-1}$
C	$-4.69761 \cdot 10^{-4}$

Table 2. Experimental values with uncertainties and deviation from calculated values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref. (Symbol in Fig. 1)	$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref. (Symbol in Fig. 1)
293.15	818.50 ± 0.70	-0.97	1880-bru-1(×)	293.15	817.90 ± 0.60	-1.57	1940-cow/jef(×)
289.45	820.10 ± 1.00	-2.48	1893-eyk ¹⁾	334.65	784.80 ± 0.60	1.11	1940-cow/jef(×)
354.35	766.50 ± 1.00	0.36	1893-eyk(×)	361.05	763.00 ± 0.60	2.91	1940-cow/jef(×)
293.95	817.90 ± 1.00	-0.90	1895-eyk ¹⁾	253.15	854.10 ± 0.50	1.67	1941-col(◆)
297.05	815.70 ± 1.00	-0.48	1895-eyk ¹⁾	273.15	836.80 ± 0.50	0.66	1941-col(◆)
410.65	717.70 ± 1.50	3.73	1895-eyk ¹⁾	293.15	819.40 ± 0.50	-0.07	1941-col(◆)
411.55	716.80 ± 1.50	3.69	1895-eyk ¹⁾	313.15	802.10 ± 0.50	-0.33	1941-col(◆)
290.65	821.10 ± 0.60	-0.48	1909-fal(×)	333.15	784.80 ± 0.50	-0.21	1941-col(◆)
300.95	813.30 ± 0.60	0.43	1909-fal(×)	353.15	767.00 ± 0.50	-0.22	1941-col(◆)
310.05	805.10 ± 0.60	0.00	1909-fal(×)	373.15	748.80 ± 0.50	-0.25	1941-col(◆)
319.45	797.30 ± 0.60	0.32	1909-fal(×)	393.15	729.90 ± 0.50	-0.60	1941-col(◆)
326.65	791.20 ± 0.70	0.49	1909-fal(×)	413.15	711.10 ± 0.50	-0.48	1941-col(◆)
334.65	784.40 ± 0.70	0.71	1909-fal(×)	433.15	692.10 ± 0.50	-0.18	1941-col(◆)
342.85	777.30 ± 0.70	0.87	1909-fal(×)	293.15	818.70 ± 0.60	-0.77	1952-coo(×)
273.15	835.45 ± 0.60	-0.69	1931-def(×)	298.15	814.86 ± 0.30	-0.39	1993-com/fra(□)
288.15	823.30 ± 0.60	-0.38	1931-def(×)	298.15	814.34 ± 0.40	-0.91	1995-com/fra(Δ)
303.15	811.05 ± 0.60	0.05	1931-def(×)	298.15	815.66 ± 0.40	0.41	1995-com/fra-2(○)
288.15	822.66 ± 0.60	-1.02	1936-ceu(×)	298.15	815.56 ± 0.50	0.31	1995-com/fra-4(∇)
303.15	810.21 ± 0.60	-0.79	1936-ceu(×)				

¹⁾ Not included in Fig. 1.

Further references: [1857-sta, 1883-sch-3, 1888-beh-1, 1914-low, 1919-eyk, 1927-kir-1, 1928-car/adk, 1932-ver/glo, 1938-tho/cam, 1950-naz/fis, 1954-doo, 1954-hil/sen, 1963-iva/dol].

cont.

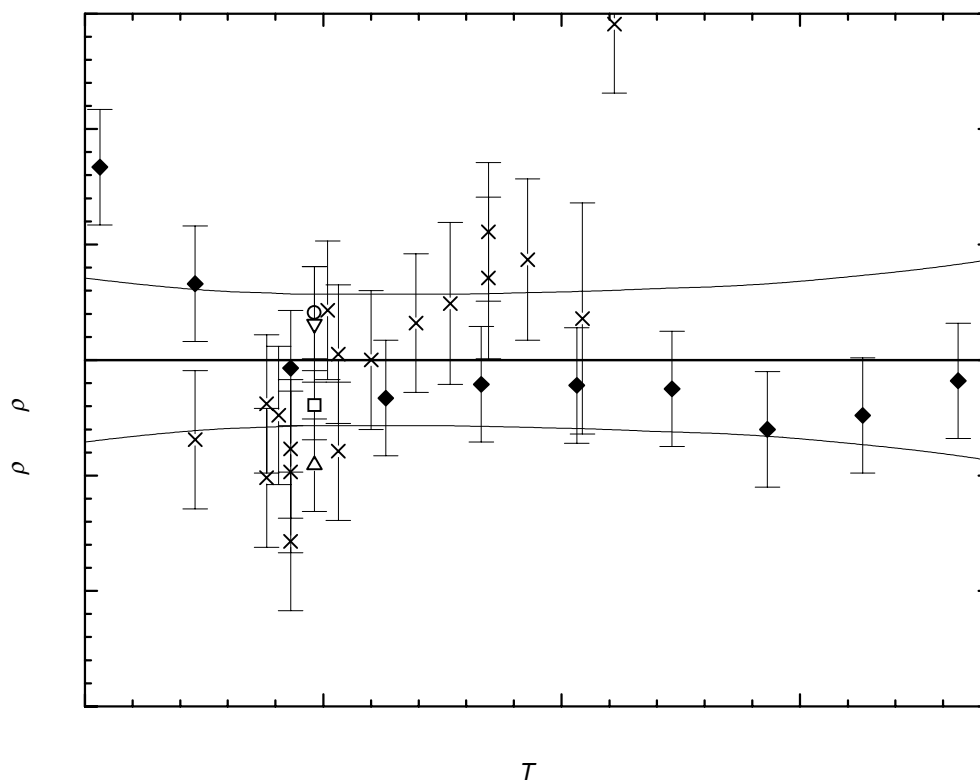


Fig. 1. The symbols show the deviation of the calculated from the experimental values from Table 2. The curves above and below the zero line indicate the calculated error region of the recommended values given in Table 3. The error bars represent the experimental errors. (Error bars smaller than the symbols are omitted for clarity of the figure.)

Table 3. Recommended values (fit to the reliable experimental values according to the equations $\rho = A + BT + CT^2 + DT^3 + \dots$ or $\rho = [1 + 1.75(1 - T/T_c)^{1/3} + 0.75(1 - T/T_c)][\rho_c + A(T_c - T) + B(T_c - T)^2 + C(T_c - T)^3 + D(T_c - T)^4]$).

$\frac{T}{\text{K}}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{T}{\text{K}}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{T}{\text{K}}$	$\frac{\rho \pm \sigma_{\text{fit}}}{\text{kg} \cdot \text{m}^{-3}}$
250.00	854.96 ± 0.71	310.00	805.14 ± 0.57	390.00	733.45 ± 0.65
260.00	846.89 ± 0.66	320.00	796.51 ± 0.57	400.00	724.06 ± 0.68
270.00	838.73 ± 0.62	330.00	787.78 ± 0.57	410.00	714.59 ± 0.72
280.00	830.47 ± 0.59	340.00	778.96 ± 0.58	420.00	705.01 ± 0.76
290.00	822.12 ± 0.58	350.00	770.05 ± 0.59	430.00	695.35 ± 0.81
293.15	819.47 ± 0.57	360.00	761.04 ± 0.60	440.00	685.59 ± 0.87
298.15	815.25 ± 0.57	370.00	751.93 ± 0.62		
300.00	813.68 ± 0.57	380.00	742.74 ± 0.63		

4-Octanone

[589-63-9]

**MW = 128.21****206****Table 1.** Fit with estimated *B* coefficient for 5 accepted points. Deviation $\sigma_w = 0.268$.

Coefficient	$\rho = A + BT$
<i>A</i>	1065.17
<i>B</i>	-0.840

Table 2. Experimental values with uncertainties and deviation from calculated values.

$\frac{T}{K}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
297.95	814.6 ± 1.0	-0.29	1942-owe/qua
308.00	806.5 ± 1.0	0.05	1942-owe/qua
323.30	793.9 ± 1.0	0.30	1942-owe/qua
293.15	818.6 ± 1.0	-0.33	1950-naz/fis
293.15	819.2 ± 1.0	0.27	1965-shu/kar

Table 3. Recommended values.

$\frac{T}{K}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$
290.00	821.6 ± 1.1
293.15	818.9 ± 1.1
298.15	814.7 ± 1.0
310.00	804.8 ± 1.0
320.00	796.4 ± 1.3
330.00	788.0 ± 1.6

2,2,4-Trimethyl-3-pentanone

[5857-36-3]

**MW = 128.21****207****Table 1.** Fit with estimated *B* coefficient for 7 accepted points. Deviation $\sigma_w = 0.733$.

Coefficient	$\rho = A + BT$
<i>A</i>	1076.40
<i>B</i>	-0.920

Table 2. Experimental values with uncertainties and deviation from calculated values.

$\frac{T}{K}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.	$\frac{T}{K}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	$\frac{\rho_{\text{exp}} - \rho_{\text{calc}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
273.15	823.9 ± 1.0	-1.23	1913-fav	298.15	802.3 ± 0.6	0.19	1947-how/mea
293.15	806.1 ± 1.0	-0.59	1913-fav	293.15	805.1 ± 0.6	-1.60	1960-pet/sok
298.15	805.3 ± 3.0	3.24	1913-hal/bau ¹⁾	293.15	807.2 ± 0.4	0.50	1970-sel
298.15	804.3 ± 2.0	2.22	1931-pfe/adk ¹⁾	298.15	802.6 ± 0.4	0.50	1970-sel
293.15	806.5 ± 0.6	-0.16	1947-how/mea				

¹⁾ Not included in calculation of linear coefficients.

cont.

Table 3. Recommended values.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$
270.00	828.0 ± 1.5
280.00	818.8 ± 1.1
290.00	809.6 ± 0.9
293.15	806.7 ± 0.9
298.15	802.1 ± 0.9

3,3,4-Trimethyl-2-pentanone

[5340-47-6]

C₈H₁₆O

MW = 128.21

208**Table 1.** Experimental value with uncertainty.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
293.15	839.5 ± 0.6	1942-eny

3,4,4-Trimethyl-2-pentanone

[5340-45-4]

C₈H₁₆O

MW = 128.21

209**Table 1.** Experimental value with uncertainty.

$\frac{T}{\text{K}}$	$\frac{\rho_{\text{exp}} \pm 2\sigma_{\text{est}}}{\text{kg} \cdot \text{m}^{-3}}$	Ref.
293.15	826.0 ± 2.0	1934-dra/kli